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Boulder Laboratories

A COMPILATION OF THE PHYSICAL EQUILIBRIA AND RELATED PROPERTIES OF THE HYDROGEN-NITROGEN SYSTEM

BY D. E. DRAYER AND T. M. FLYNN



U. S. DEPARTMENT OF COMMERCE NATIONAL BUREAU OF STANDARDS

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May 1961

A Compilation of the

Physical Equilibria and Related Properties

of the

Hydrogen - Nitrogen System

by

Dennis E. Drayer

and

Thomas M. Flynn

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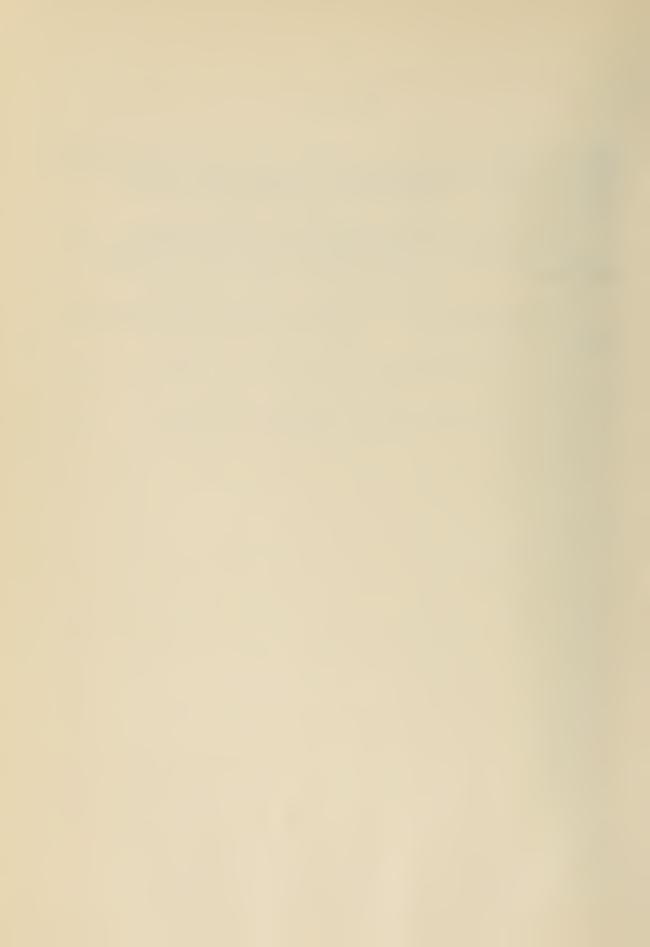
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Abstract

Published data have been used to calculate K factors for the hydrogen-nitrogen system over the liquid-vapor range of 68.2 to 122.2°K, and 10 to 225 atmospheres. K factors are presented graphically for eleven isotherms within this range.

Published data on the solid-gas and solid-liquid regions are presented separately as composition versus pressure at constant temperature.

A bibliography of 250 references pertaining to the hydrogennitrogen system is included.



1. Introduction

1.1 Purpose

Hydrogen gas for liquefaction frequently contains large amounts of other gases. Purification of these various hydrogen sources requires considerable knowledge of the physical equilibria of the systems involved. Many theoretical studies have attempted to explain and predict the non-ideal behavior of these systems with varying degrees of success.

An initial step in the study of physical equilibria logically demands a review of current knowledge. In this, the first of a series, the hydrogen-nitrogen system is examined. The purpose of this paper is to determine what is known about the physical equilibria relationships and to present a thorough compilation of known related data for this system. It is hoped that this paper will thus provide a firm basis for the conduct of related research programs and place in the hands of the design engineer the "best" information now available.

Future publications in this area will be concerned with the physical equilibira of hydrogen and other important components.

1.2 Organization

The information is presented in three principal parts: (1) physical equilibria with major emphasis on vapor-liquid equilibria, (2) properties related to physical equilibria, and (3) a bibliography of references. Some discussion is presented with Part (1). The information of Part (2) is presented in tabular form, including the source of the data. Part (3), the Bibliography, lists the references alphabetically by the first author.

1.3 Scope

The scope of this work is as follows: a thorough literature search, as summarized in NBS Technical Note No. 56, revealed much of the pertinent data; such data were abstracted and presented in the form of K-factor charts and as a bibliography of references for related areas of interest. The lists searched are presented in the above reference and will not be enumerated here. They were, however, brought up to date, July 1960.

1.4 Acknowledgements

The authors especially appreciate the aid of the staff of the Data Center of the National Bureau of Standards Cryogenic Engineering Laboratory, who provided the majority of the original papers for review.

2. Survey of Literature

The literature search revealed six important references for hydrogen-nitrogen vapor-liquid equilibria. There were Akers and Eubanks (4), Gonikberg, et al. (91), Maimoni (166), Ruhemann and Zinn (212), Steckel and Zinn (225), and Verschoyle (236). K-factor charts were prepared from data taken from these references. In all but two cases (4, 166), the data had to be re-interpreted to arrive at K-factors.

Two important sources of solid-gas and solid-liquid data were found. These were Dokoupil et al. (57) and Petit (196). This information is presented separately as charts of concentration versus pressure at constant temperatures.

No related physical data are presented in this report; only the references for such material are listed. Other areas so covered include adsorption, diffusion, purification processes, solubility relationships, density and compressibility data, equations of state, thermodynamic and transport properties, P-V-T data, critical constants, virial coefficients, Beattie-Bridgeman constants, techniques of analyses, and various processing references. Such material for the pure components as well as for mixtures of hydrogen and nitrogen is included in many cases.

3. Discussion of Available Data

For this system one could expect the vapor-liquid data, if complete, to range roughly from the triple point temperature of nitrogen to the critical temperature of nitrogen (63.1° to 126.2° K). The references presented in this report provided data for eleven isotherms between 63.2°K to 122.2°K. The isotherms so presented are 63.2°, 68.2°, 78°-79°, 83.3°, 88.2°, 90°, 95°-95.4°, 107.7°, 109°, 113° and 122.2°K. (Rather than take an average temperature

for the 78°-79°, 83°-83.3°, and 95°-95.4°K values, the equilibria data for each narrow range are plotted as one isotherm.) Thus, the data available do present a rather complete picture of the vapor-liquid equilibria for this binary system.

The solid-liquid region has been explored from 20° to 32°K and from 12 to 35 atmospheres. The solid-vapor region has been explored from 25° to 70°K and from 1.3 to 50 atmospheres.

The P-T region covered by published data is presented in Figure 1. This figure indicates that this system has been rather thoroughly explored by the several investigators. (The data for the hydrogen P-T diagram were taken from Johnson (122) and from Woolley, Scott and Brickwedde (248). The data for the nitrogen P-T diagram were also taken from the former reference).

The original data were treated to arrive at the corresponding K-factors. K is defined as y/x where y is the mole fraction of one component in the vapor phase and x is the mole fraction of that component in the condensed phase. K-factors were calculated for each component as a function of pressure and temperature. After plotting the K-factors derived from the various investigators, a smooth curve was drawn for the given isotherm. Finally, the smoothed individual K-factors were transferred to a plot of K versus pressure with temperature as a parameter.

It is not the purpose of this report to present a test of the data for thermodynamic consistency. Maimoni (166) has performed such tests with much of the data herein presented. Maimoni has corrected Verschoyle's data by using new values for the vapor pressure of nitrogen. In this article the original data of Verschoyle are given. As pointed out also by Maimoni, the data of Ruhemann and Zinn differ appreciably from other published values.

Of the data analyzed, the K-factor at the lower pressures showed the most scatter. This was true primarily for the hydrogen K-factor; less scatter was noted for the nitrogen K-factor. Undoubtedly this stems partly from the analytical techniques used.

It must be emphasized that this report is based entirely on the original data of the investigators. These data, in some cases, have not been tested for thermodynamic consistency, and should be used only with thorough awareness of this fact.

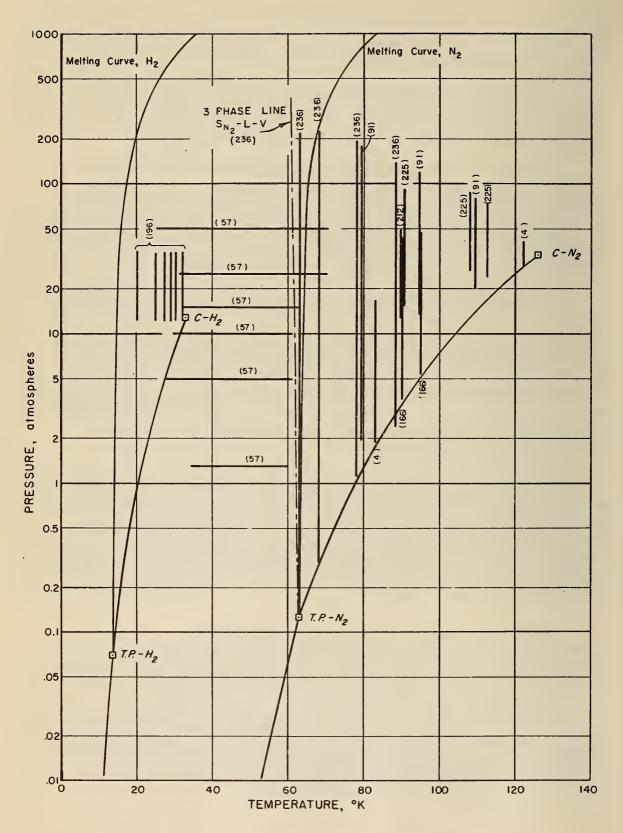


Figure 1. Regions Covered by Published Data

4. K-Factor Charts

Presented in Tables I through VII in the Appendix are the data used in computing K-factors.

Figures 2 and 3 are plots of the K-factors of hydrogen and nitrogen, respectively. Dotted portions on these figures indicate extrapolated areas. (These extrapolations were performed mainly by the original authors.) Figure 4 shows, finally, the curves for both hydrogen and nitrogen as taken from Figures 2 and 3. In Figure 4, hydrogen K-factors are situated above the line K = 1, and nitrogen K-factors are below this line. The significance of the fact that the two curves meet at K = 1 is a characteristic of the plait point. (Verschoyle discusses the plait point.) Thus, the line K = 1 represents a locus of the plait points. The plait point for the 68.2°K isotherm, not shown in Figure 4, was estimated by Verschoyle to be at 340 atmospheres.

The use of these charts might be as follows: for a given system pressure and temperature, K-factors could be read from Figure 4 and the phase compositions found by the following equations.

$$K_1 = y_1/x_1 \tag{1}$$

$$K_2 = y_2/x_2 \tag{2}$$

$$x_1 + x_2 = 1.0$$
 (3)

$$y_1 + y_2 = 1.0$$
 (4)

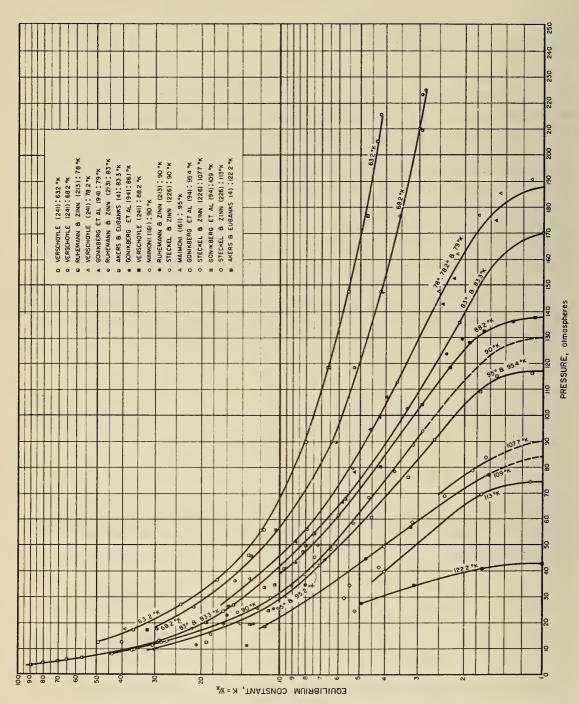
where the subscripts 1 and 2 refer to hydrogen and nitrogen. As an example, one might wish to calculate the phase compositions at 88.2°K and 100 atm. Here

$$K_{H_2} = 3.14 = (y/x)_{H_2}$$
; $y_{H_2} = 3.14 x_{H_2}$

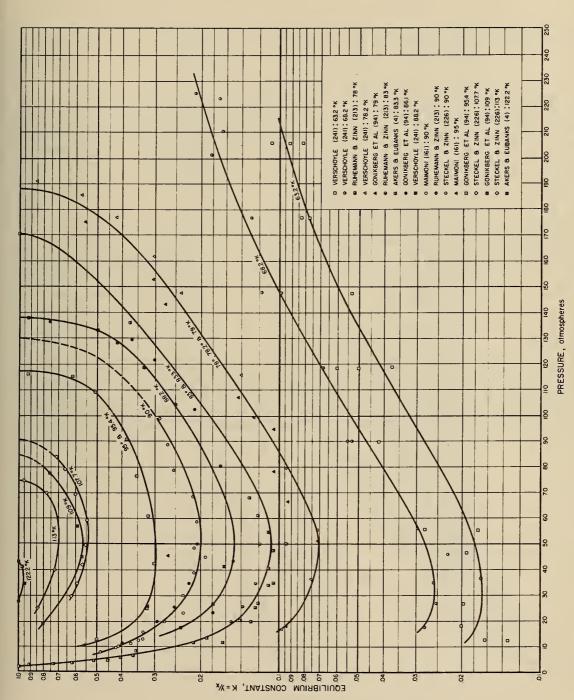
$$K_{N_2} = 0.235 = (y/x)_{N_2}$$
; $y_{N_2} = 0.235x_{N_2}$

Solving equations (3) and (4) for the phase composition gives

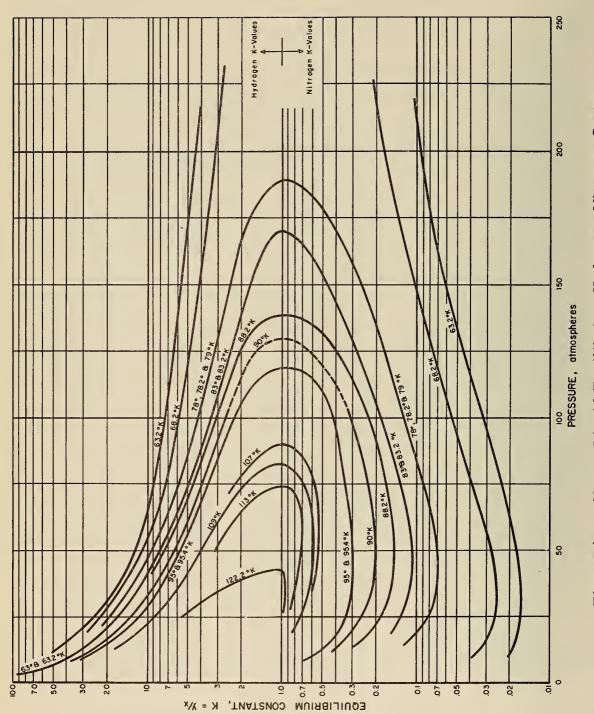
$$y_{H_3} = 0.827$$
 $x_{H_2} = 0.263$



Hydrogen-Nitrogen Vapor-Liquid Equilibria Data. Hydrogen K-Factors Figure 2.



Hydrogen-Nitrogen Vapor-Liquid Equilibria Data. Nitrogen K-Factors Figure 3.



Vapor-Liquid Equilibria. Hydrogen-Nitrogen System Figure 4.

$$y_{N_2} = 0.173$$
 $x_{N_2} = 0.737$

Similarly, dew points and bubble points of given hydrogen-nitrogen mixtures can be calculated.

The critical constants as derived from the various isotherms are not shown on any of the figures. Verschoyle does comment about the critical points for his isotherms. Table II lists his critical constants.

5. Solid-Liquid Equilibria

Shown in Table VIII are the data of Petit (196). Six isotherms relating liquid phase composition and system pressure are shown in Figure 5.

6. Solid-Gas Equilibria

The data of Dokoupil, Van Soest, and Swenker (57) are given in Table IX. The data have been plotted to derive gas phase composition as related to total pressure for eight isotherms between 25° and 60° K. Table X presents the data in this form. Figure 6 is a plot of the data of Table X.

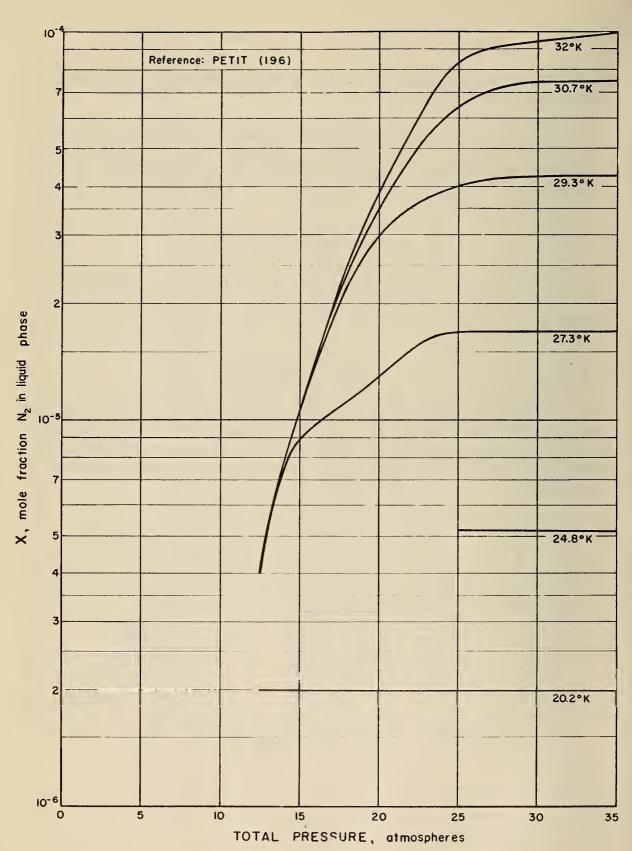


Figure 5. Solid-Liquid Equilibria. Concentration of Nitrogen in the Liquid Phase

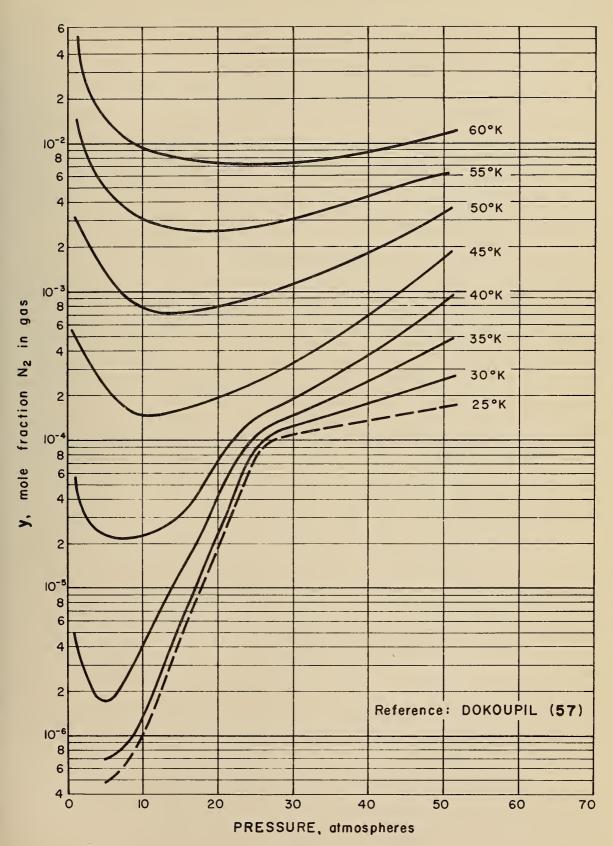


Figure 6. Solid-Vapor Equilibria. Concentration of Nitrogen in the Vapor Phase



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Phenomena Index



Phenomenon

MAJOR COMPONENT HYDROGEN

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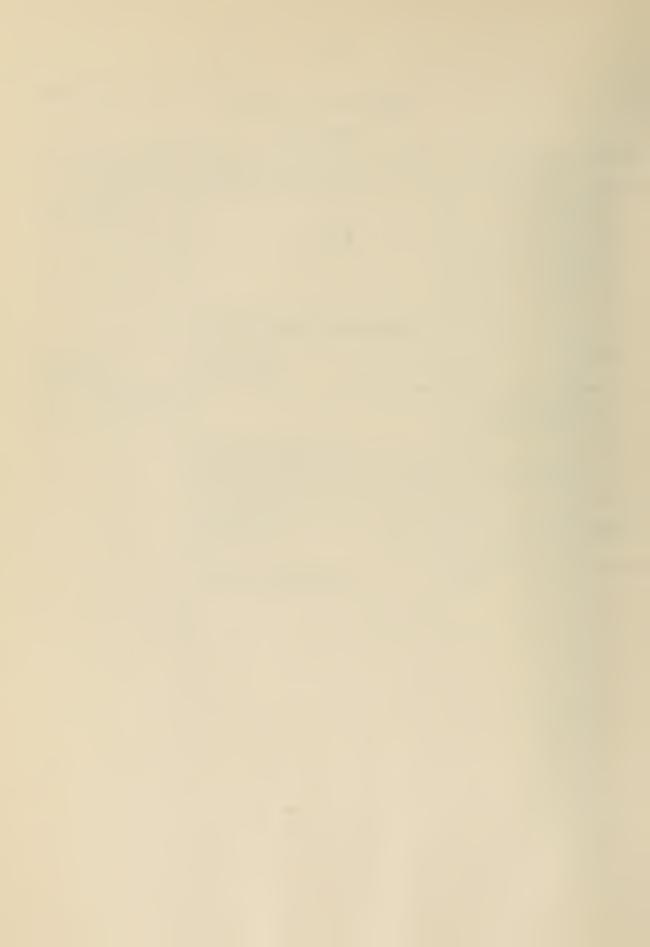
Phenomenon

MAJOR COMPONENT

NITROGEN				
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Properties

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Processes

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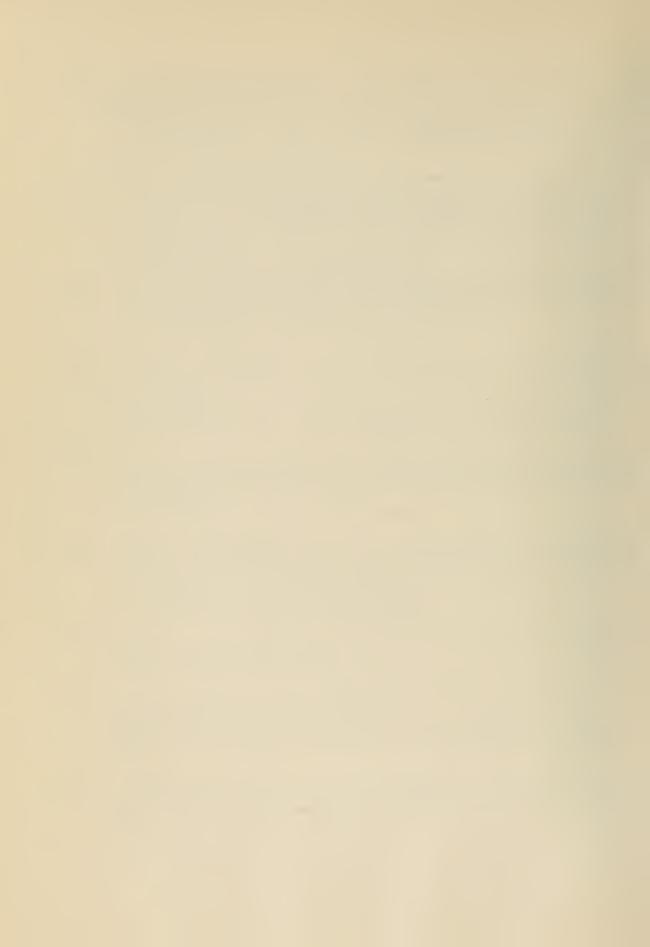
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11.0

Appendix



Table I

$N_2^-H_2^-$ PRESSURE-CONCENTRATION DATA

Reference: Verschoyle (236)

C	Tempe	Temperature Pressure		Li	quid	Vaj	oor	К		
185 88, 2 137, 73 47, 0 53, 0 50, 8 49, 2 1, 08 0, 928	_		-							
	<u> </u>	<u> </u>	Aun	Wille 70 112	Wille /6 14 2	Widle /6 11 ₂	Widle /6 142	112	1,72	
	-185	88. 2	137. 73	47.0	53.0	50. 8	49. 2	1.08	0. 928	
	- 11		132, 81	42.0	58.0	71.2	28.8	1.69	0.497	
	0	- 11	128.08	38.7	61.3	74. 5	25. 5	1.92	0.416	
		"	118.34	34. 5	65. 5	78. 3	21.7	2.27	0.331	
			104.00	28.3	71.7	82. 1	17.9	2. 90	0. 250	
10	"		80.00	20.7	79. 3	86.6	13.4	4.18	0.169	
17, 01 2,4 97,6 77,0 23,0 32,1 0,236 -195 78,2 190,89 54,9 45,1 61,7 38,3 1,12 0,849		- 11	41.04	9, 2	90.8	85. 3	14.7	9. 27	0.162	
195 78.2 190.89 54.9 45.1 61.7 38.3 1.12 0.849	"	- 11	26. 76	5, 3	94.7	83.3	16.7	15.7	0.176	
	11	"	17.01	2.4	97.6	77.0	23.0	32, 1	0. 236	
	105	70 3	100.00	54.0	45.1	41.7	20.2	1 12	0.040	
			13. 11.			i		1		
			1					1		
10.166										
" 113.60 24.8 75.2 89.5 10.5 3.61 0.140 " 79.90 17.5 82.5 92.2 7.8 5.27 0.0945 " 155.56 11.9 88.1 93.7 6.3 7.87 0.0715 " 17.19 2.3 97.7 90.5 9.5 39.3 0.0972 -205 68.2 224.81 31.1 68.9 85.4 14.6 2.75 0.212 " " 210.28 29.6 70.4 88.3 11.7 2.98 0.166 " " 209.28 29.6 70.4 88.3 11.7 2.98 0.166 " " 209.28 29.6 70.4 87.0 13.0 2.94 0.185 " " 176.40 25.2 74.8 90.3 9.7 3.58 0.130 " " 147.41 21.9 78.1 92.2 7.8 4.21 0.100 " " 1847.41 21.9 78.1 92.2 7.8 4.21 0.100 " " 89.67 14.7 85.3 95.3 4.7 6.48 0.0551 " " 89.67 14.7 85.3 95.3 4.7 6.48 0.0551 " " 55.88 9.4 90.6 97.3 2.7 10.4 14.8 0.0257 " " 17.19 3.3 96.7 97.6 2.4 11.2 9 0.0252 " " " 17.19 3.3 96.7 97.3 2.7 10.4 14.8 0.0257 " " 17.19 3.3 96.7 97.3 2.7 10.4 14.8 0.0257 " " 17.19 3.3 96.7 97.3 2.7 2.9 5 0.0279 -210 63.2 215.12 22.2 77.8 92.9 7.1 4.18 0.018 " " 17.19 3.3 96.7 97.3 2.7 2.9 5 0.0279 -210 63.2 215.12 22.2 77.8 92.9 7.1 4.18 0.018 " " 17.19 3.3 96.7 97.3 2.7 2.9 5 0.0259 " " 18.48 14.6 85.4 99.5 93.3 6.7 4.7 0.0298 " " 17.19 3.3 96.7 97.3 2.7 10.4 14.8 0.0257 " " 18.48 14.6 85.4 99.6 79.6 2.4 14.8 0.0257 " " 18.48 14.6 85.4 99.6 79.6 2.4 14.8 0.0257 " " 18.48 14.6 85.4 99.5 93.3 6.7 4.7 0.0298 " " 17.64 118.4 14.7 85.3 95.7 4.3 5.56 0.018 " " 18.49 14.4 14.7 85.3 95.7 4.3 5.56 0.0519 " " 18.48 14.6 85.4 99.5 7.6 92.9 7.1 4.18 0.0913 " " 18.48 14.6 85.4 99.5 7.6 93.3 6.7 4.79 0.0832 " " 18.48 14.6 19.5 80.5 93.3 6.7 4.79 0.0832 " " 18.49 14.79 19.5 80.5 93.3 6.7 4.79 0.0832 " " 18.48 14.6 14.7 85.3 95.7 4.3 5.56 0.0519 " " 18.48 14.6 14.7 85.3 95.7 4.3 5.56 0.0519 " " 18.48 14.6 14.7 85.3 95.7 4.8 5.2 6.63 0.0607 " " 18.46 11.75 92.5 98.2 18.8 13.1 0.0194 " " 17.640 17.2 82.8 95.7 4.8 5.2 6.63 0.0607 " " 18.55.50 8.5 91.5 98.2 18.8 13.1 0.0194 " " 17.70 92.7 97.3 98.0 2.0 36.3 3.9 0.0194 " " 17.70 92.7 97.3 98.0 2.0 36.3 3.9 0.0194 " " 17.70 92.7 97.3 98.0 2.0 36.3 3.9 0.0194										
1.									1	
	4								1	
					10.00			1	i	
-205 68, 2 224, 81 31, 1 68, 9 85, 4 14, 6 2, 75 0, 212 " 210, 28 29, 6 70, 4 88, 3 11, 7 2, 98 0, 166 " 170, 40 25, 2 74, 8 90, 3 9, 7 3, 58 0, 130 " 147, 44 22, 0 78, 0 90, 8 9, 2 4, 13 0, 118 " 147, 41 21, 9 78, 1 92, 2 7, 8 4, 21 0, 100 " 18, 47 18, 1 81, 9 94, 4 5, 6 5, 22 0, 0684 " " 89, 67 14, 7 85, 3 95, 3 4, 7 6, 48 0, 0551 " " 55, 88 9, 4 90, 6 97, 3 2, 7 10, 4 0, 0298 " " 45, 89 7, 6 92, 4 97, 9 2, 1 12, 9 0, 0227 " " 35, 98 6, 6 93, 4 97, 6 2, 4 14, 8 0, 0257 " " 171, 19 3, 3 96, 7 97, 3 2, 7 29, 5 0, 0279 " " 171, 19 3, 3 96, 7 97, 3 2, 7 29, 5 0, 0279 " " 205, 46 21, 6 78, 4 93, 5 6, 5 4, 36 0, 108 " " 176, 40 19, 5 80, 5 93, 3 6, 7 4, 79 0, 0832 " " 176, 40 19, 5 80, 5 93, 3 6, 7 4, 79 0, 0832 " " 176, 40 19, 5 80, 5 93, 3 6, 7 4, 79 0, 0832 " " 176, 40 19, 5 80, 5 93, 3 6, 7 4, 79 0, 0832 " " 176, 40 19, 5 80, 5 93, 3 6, 7 4, 79 0, 0832 " " 176, 40 19, 5 80, 5 93, 3 6, 7 4, 79 0, 0832 " " 176, 40 19, 5 80, 5 93, 3 6, 7 4, 79 0, 0832 " " 176, 40 19, 5 80, 5 93, 3 6, 7 4, 79 0, 0832 " " 18, 48, 41, 6 85, 4 96, 8 3, 2 6, 63 0, 0379 " " 118, 48, 14, 6 85, 4 96, 8 3, 2 6, 63 0, 0379 " " 118, 48, 14, 6 85, 4 96, 8 3, 2 6, 63 0, 0379 " " 118, 44, 14, 7 85, 3 95, 7 4, 3 5, 56 0, 019 " " 155, 50 8, 3 91, 7 98, 4 1, 6 11, 9 0, 0174 " " 55, 50 8, 3 91, 7 98, 4 1, 6 11, 9 0, 0174 " " 55, 50 8, 3 91, 7 98, 4 1, 6 17, 3 0, 0174 " " 46, 11 7, 5 92, 5 98, 2 1, 8 13, 1 0, 0194 " " 170, 9 2, 7 97, 3 98, 0 2, 0 36, 3 0, 0206 " " 12, 21 2, 25 97, 5 98, 4 1, 6 17, 3 0, 0179 " " 170, 9 2, 7 97, 3 98, 0 2, 0 36, 3 0, 0206 " " 12, 21 2, 25 97, 5 98, 4 1, 6 17, 3 0, 0194									l .	
"			17.19	2, 3	97. 7	90.5	9. 5	39.3	0.0972	
"						85.4		2. 75	0. 212	
				30. 7	69.3	88. 1	11.9	2.87	0.172	
					70.4	88. 3	11.7	2.98	0.166	
			209. 28	29.6	70.4	87. 0	13.0	2. 94	0.185	
			176.40	25. 2	74.8	90. 3	9. 7	3. 58	0.130	
	1		147. 44	22.0	78.0	90.8	9. 2	4.13	0.118	
			147.41	21.9	78.1	92. 2	7.8	4. 21	0.100	
			118.47	18.1	81.9	94. 4	5. 6	5. 22	0.0684	
	1		89.67	14.7	85. 3	95. 3	4.7	6.48	0.0551	
			89. 55	15.4	84.6	95.5	4.5	6.20	0.0532	
35. 98 6. 6 93. 4 97. 6 2. 4 14. 8 0. 0257 26. 58 4. 6 95. 4 97. 6 2. 4 21. 2 0. 0252 17. 19 3. 3 96. 7 97. 3 2. 7 29. 5 0. 0279 -210 63. 2 215. 12 22. 2 77. 8 92. 9 7. 1 4. 18 0. 0913 205. 46 21. 6 78. 4 93. 5 6. 5 4. 33 0. 0829 "" 205. 41 21. 0 79. 0 91. 5 8. 5 4. 36 0. 108 "" 176. 43 18. 9 81. 1 93. 7 6. 3 4. 96 0. 0777 "" 176. 40 19. 5 80. 5 93. 3 6. 7 4. 79 0. 0832 "" 147. 40 17. 2 82. 8 95. 7 4. 3 5. 56 0. 0519 "" 118. 48 14. 6 85. 4 96. 8 3. 2 6. 63 0. 0375 "" 118. 44 14. 7 85. 3 95. 7 4. 3 6. 51 0. 0504 "" 189. 58 12. 0 88. 0 96. 3 3. 7 8. 02 0. 0420 "" 19 55. 59 8. 5 91. 5 97. 4 2. 6 11. 5 0. 0284 "" 10 46. 11 7. 5 92. 5 98. 2 1. 8 13. 1 0. 0194 "" 36. 30 5. 7 94. 3 98. 4 1. 6 17. 3 0. 0170 "" 26. 70 4. 1 95. 9 98. 1 1. 9 23. 9 0. 0198 "" 17. 09 2. 7 97. 3 98. 0 2. 0 36. 3 0. 0206 "" " 20. 225 "" 12. 2 1 2. 5 97. 5 98. 4 1. 6 39. 4 0. 0164					j	97.3	2,7	10.4	0.0298	
" 26.58					92.4	97. 9	2. 1	12.9	0. 0227	
17.19 3.3 96.7 97.3 2.7 29.5 0.0279 -210 63.2 215.12 22.2 77.8 92.9 7.1 4.18 0.0913 -210 63.2 205.46 21.6 78.4 93.5 6.5 4.33 0.0829	1 1		35. 98	6.6	93. 4	97. 6	2.4	14.8	0.0257	
-210 63. 2 215. 12 22. 2 77. 8 92. 9 7. 1 4. 18 0. 0913 " " 205. 46 21. 6 78. 4 93. 5 6. 5 4. 33 0. 0829 " " 205. 41 21. 0 79. 0 91. 5 8. 5 4. 36 0. 108 " " 176. 43 18. 9 81. 1 93. 7 6. 3 4. 96 0. 0777 " " 176. 40 19. 5 80. 5 93. 3 6. 7 4. 79 0. 0832 " " 147. 40 17. 2 82. 8 95. 7 4. 3 5. 56 0. 0519 " " 118. 48 14. 6 85. 4 96. 8 3. 2 6. 63 0. 0375 " " 118. 44 14. 7 85. 3 95. 7 4. 3 6. 51 0. 0504 " " 89. 58 12. 0 88. 0 96. 3 3. 7 8. 02 0. 0420 " " 55. 59 8. 5 91. 5 97. 4 2. 6 11. 5 0. 0284 " " 46. 11 7. 5 92. 5 98. 2 1. 8 13. 1 0. 0194 " " 36. 30 5. 7 94. 3 98. 4 1. 6 17. 3 0. 0170 " " 26. 70 4. 1 95. 9 98. 1 1. 9 23. 9 0. 0198 " " 17. 09 2. 7 97. 3 98. 0 2. 0 36. 3 0. 0206 " " 17. 09 2. 7 97. 3 98. 0 2. 0 36. 3 0. 0206			26. 58	4.6	95. 4	97.6	2.4	21.2	0.0252	
""" 205.46 21.6 78.4 93.5 6.5 4.33 0.0829 """ 205.41 21.0 79.0 91.5 8.5 4.36 0.108 """ 176.43 18.9 81.1 93.7 6.3 4.96 0.0777 """ 176.40 19.5 80.5 93.3 6.7 4.79 0.0832 """ 147.40 17.2 82.8 95.7 4.3 5.56 0.0519 """ 118.48 14.6 85.4 96.8 3.2 6.63 0.0375 """ 118.44 14.7 85.3 95.7 4.3 6.51 0.0504 """ 118.41 14.3 85.7 94.8 5.2 6.63 0.0607 """ 89.58 12.0 88.0 96.3 3.7 8.02 0.0420 """ 55.59 8.5 91.5 97.4 2.6 11.5 0.0284 """ 55.50 8.3 91.7 98.4 1.6 11.9 0.0174 """ 46.11	"	11	17.19	3. 3	96. 7	97.3	2.7	29. 5	0.0279	
" 205.41 21.0 79.0 91.5 8.5 4.36 0.108 " 176.43 18.9 81.1 93.7 6.3 4.96 0.0777 " 176.40 19.5 80.5 93.3 6.7 4.79 0.0832 " 147.40 17.2 82.8 95.7 4.3 5.56 0.0519 " 118.48 14.6 85.4 96.8 3.2 6.63 0.0375 " 118.44 14.7 85.3 95.7 4.3 6.51 0.0504 " " 118.41 14.3 85.7 94.8 5.2 6.63 0.0607 " " 89.58 12.0 88.0 96.3 3.7 8.02 0.0420 " " 55.59 8.5 91.5 97.4 2.6 11.5 0.0284 " " 55.50 8.3 91.7 98.4 1.6 11.9 0.0174 " 46.11 7.5 92.5 98.2 1.8 13.1 0.0194 " " 36.30 5.7 94.3 98.4 1.6 17.3 0.0170 " " 26.70 4.1 95.9 98.1 1.9 23.9 0.0198 " " 17.09 2.7 97.3 98.0 2.0 36.3 0.0206 " " 12.21 2.5 97.5 98.4 1.6 39.4 0.0164	-210	63. 2	215.12	22. 2	77.8	92.9	7. 1	4.18	0. 0913	
""" 205.41 21.0 79.0 91.5 8.5 4.36 0.108 """ 176.43 18.9 81.1 93.7 6.3 4.96 0.0777 """ 176.40 19.5 80.5 93.3 6.7 4.79 0.0832 """ 147.40 17.2 82.8 95.7 4.3 5.56 0.0519 """ 118.48 14.6 85.4 96.8 3.2 6.63 0.0375 """ 118.44 14.7 85.3 95.7 4.3 6.51 0.0504 """ 118.41 14.3 85.7 94.8 5.2 6.63 0.0607 """ 89.58 12.0 88.0 96.3 3.7 8.02 0.0420 """ 89.58 12.0 88.0 96.3 3.7 8.02 0.0420 """ 55.59 8.5 91.5 97.4 2.6 11.5 0.0284 """ 55.59 8.3 91.7 98.4 1.6 11.9 0.0174 """ 46.11	11	11	205.46	21.6	78. 4	93.5	6. 5	4.33	0. 0829	
""" 176, 40 19.5 80.5 93.3 6.7 4.79 0.0832 """ 147, 40 17.2 82.8 95.7 4.3 5.56 0.0519 """ 118.48 14.6 85.4 96.8 3.2 6.63 0.0375 """ 118.44 14.7 85.3 95.7 4.3 6.51 0.0504 """ 118.41 14.3 85.7 94.8 5.2 6.63 0.0607 """ 89.58 12.0 88.0 96.3 3.7 8.02 0.0420 """ 55.59 8.5 91.5 97.4 2.6 11.5 0.0284 """ 55.50 8.3 91.7 98.4 1.6 11.9 0.0174 """ 46.11 7.5 92.5 98.2 1.8 13.1 0.0194 """ 36.30 5.7 94.3 98.4 1.6 17.3 0.0170 """ 26.70 4.1 95.9 98.1 1.9 23.9 0.0198 """ 17.09		11	205.41	21.0	79.0	91.5	8. 5	4. 36	0.108	
""" 176,40 19.5 80.5 93.3 6.7 4.79 0.0832 """ 147.40 17.2 82.8 95.7 4.3 5.56 0.0519 """ 118.48 14.6 85.4 96.8 3.2 6.63 0.0375 """ 118.44 14.7 85.3 95.7 4.3 6.51 0.0504 """ 118.41 14.3 85.7 94.8 5.2 6.63 0.0607 """ 89.58 12.0 88.0 96.3 3.7 8.02 0.0420 """ 55.59 8.5 91.5 97.4 2.6 11.5 0.0284 """ 55.50 8.3 91.7 98.4 1.6 11.9 0.0174 """ 46.11 7.5 92.5 98.2 1.8 13.1 0.0194 """ 36.30 5.7 94.3 98.4 1.6 17.3 0.0170 """ 26.70 4.1 95.9 98.1 1.9 23.9 0.0198 """ 17.09		11	176.43	18.9	81.1	93.7	6. 3	4.96	0.0777	
""" 118.48 14.6 85.4 96.8 3.2 6.63 0.0375 """ 118.44 14.7 85.3 95.7 4.3 6.51 0.0504 """ 118.41 14.3 85.7 94.8 5.2 6.63 0.0607 """ 89.58 12.0 88.0 96.3 3.7 8.02 0.0420 """ 55.59 8.5 91.5 97.4 2.6 11.5 0.0284 """ 55.50 8.3 91.7 98.4 1.6 11.9 0.0174 """ 46.11 7.5 92.5 98.2 1.8 13.1 0.0194 """ 36.30 5.7 94.3 98.4 1.6 17.3 0.0170 """ 26.70 4.1 95.9 98.1 1.9 23.9 0.0198 """ 17.09 2.7 97.3 98.0 2.0 36.3 0.0206 """ 12.21 2.5 97.5 98.4 1.6 39.4 0.0164	11		176, 40	19.5	80. 5	93. 3	6. 7	4. 79	0. 0832	
""" 118.48 14.6 85.4 96.8 3.2 6.63 0.0375 """ 118.44 14.7 85.3 95.7 4.3 6.51 0.0504 """ 118.41 14.3 85.7 94.8 5.2 6.63 0.0607 """ 89.58 12.0 88.0 96.3 3.7 8.02 0.0420 """ 55.59 8.5 91.5 97.4 2.6 11.5 0.0284 """ 55.50 8.3 91.7 98.4 1.6 11.9 0.0174 """ 46.11 7.5 92.5 98.2 1.8 13.1 0.0194 """ 36.30 5.7 94.3 98.4 1.6 17.3 0.0170 """ 26.70 4.1 95.9 98.1 1.9 23.9 0.0198 """ 17.09 2.7 97.3 98.0 2.0 36.3 0.0206 """ 12.21 2.5 97.5 98.4 1.6 39.4 0.0164	11	11	147.40	17. 2	82.8	95. 7	4.3	5. 56	0.0519	
""" 118.41 14.3 85.7 94.8 5.2 6.63 0.0607 """ 89.58 12.0 88.0 96.3 3.7 8.02 0.0420 """ 55.59 8.5 91.5 97.4 2.6 11.5 0.0284 """ 55.50 8.3 91.7 98.4 1.6 11.9 0.0174 """ 46.11 7.5 92.5 98.2 1.8 13.1 0.0194 """ 36.30 5.7 94.3 98.4 1.6 17.3 0.0170 """ 26.70 4.1 95.9 98.1 1.9 23.9 0.0198 """ 17.09 2.7 97.3 98.0 2.0 36.3 0.0206 """ 12.21 2.5 97.5 98.4 1.6 39.4 0.0164	0	11	118.48	14.6	85. 4	96.8	3.2	6. 63		
12.0	"	11	118.44	14.7	85. 3	95. 7	4.3	6. 51	0.0504	
12.0	- 11	"	118.41	14, 3	85.7	94.8	5. 2	6. 63	0. 0607	
""" """ 55.59 8.5 91.5 97.4 2.6 11.5 0.0284 """ 55.50 8.3 91.7 98.4 1.6 11.9 0.0174 """ 46.11 7.5 92.5 98.2 1.8 13.1 0.0194 """ 36.30 5.7 94.3 98.4 1.6 17.3 0.0170 """ 26.70 4.1 95.9 98.1 1.9 23.9 0.0198 """ 17.09 2.7 97.3 98.0 2.0 36.3 0.0206 """ 12.21 2.5 97.5 98.4 1.6 39.4 0.0164	"	**	89. 58	12.0	88.0	96.3	3. 7	8.02	0. 0420	
""" """ 55.50 8.3 91.7 98.4 1.6 11.9 0.0174 """ 46.11 7.5 92.5 98.2 1.8 13.1 0.0194 """ 36.30 5.7 94.3 98.4 1.6 17.3 0.0170 """ 26.70 4.1 95.9 98.1 1.9 23.9 0.0198 """ 17.09 2.7 97.3 98.0 2.0 36.3 0.0206 """ 12.21 2.5 97.5 98.4 1.6 39.4 0.0164		11	55. 59	8. 5	91.5	97.4	2.6			
" " 46.11 7.5 92.5 98.2 1.8 13.1 0.0194 " " 36.30 5.7 94.3 98.4 1.6 17.3 0.0170 " " 26.70 4.1 95.9 98.1 1.9 23.9 0.0198 " 17.09 2.7 97.3 98.0 2.0 36.3 0.0206 " 12.21 2.5 97.5 98.4 1.6 39.4 0.0164	"		55. 50	8. 3	91.7	98. 4				
" " 36.30 5.7 94.3 98.4 1.6 17.3 0.0170 " " 26.70 4.1 95.9 98.1 1.9 23.9 0.0198 " " 17.09 2.7 97.3 98.0 2.0 36.3 0.0206 " " 12.21 2.5 97.5 98.4 1.6 39.4 0.0164	11	0	46.11	7. 5	92. 5	98. 2	1.8			
" " 26.70 4.1 95.9 98.1 1.9 23.9 0.0198 " " 17.09 2.7 97.3 98.0 2.0 36.3 0.0206 " " 12.21 2.5 97.5 98.4 1.6 39.4 0.0164	11	11	36.30	5. 7	94. 3	98. 4				
"	11	"	26.70	4, 1	95. 9	98. 1	1.9	23.9	0.0198	
"	"	II.	17. 09	2.7	97.3	98. 0	2.0			
	11	11	12, 21	2. 5	97. 5	98. 4	1.6			
	"	H	12. 15	2. 0	98.0	98. 7	1.3	1		

Table II ${\rm N_2\text{-}H_2} \ {\rm CRITICAL} \ {\rm CONSTANTS}$

Reference: Verschoyle (236)

Temperature		Plait	Point	Critical Point of Contact			
°C	°K	Pressure Atm	Mole % H ₂	Pressure Atm	Mole % H ₂		
-185	88. 2	138	53	60	87		
-195	78. 2	191	58	50	93.5		
-205	68. 2	(340)	- <u>-</u>	35	98		
-210	63. 2			25	98. 5		

Table III

N₂-H₂ PRESSURE-CONCENTRATION DATA

Reference: Maimoni (166)

	N ₂	0.335	0.346	0.371	0.417	0.484	0.421	0.232	0.191	0.559	0.317	0.265	
X	H ₂	27.1	28.3	30.8	36.0	43.8	36.8	14.6	7.45	30. 1	12.4	6.82	
1 2	Mole % N ₂	32. 68	33, 81	36.33	40.97	47.83	41.45	22.00	16.96	55.08	29.95	23.57	
Vapor	Mole % H ₂	67.32	66.19	63. 67	59.03	52.17	58.55	78.00	83.04	44.92	70.05	76.43	
Liquid	Mole % N ₂	97.52	97.66	97.93	98.36	98.81	98.41	94.66	88.85	98.51	94.34	88. 79	
Liq	Mole % H ₂	2.48	2.34	2.07	1.64	1.19	1.59	5.34	11.15	1.49	5. 66	11.21	
Pressure	Atm	13.38	12.80	11.69	10.07	8.32	9.93	24.09	45.34	10.94	25.87	44.72	
Temperature	°K	06	Ξ	=	=	=			=	95	: =	=	

Table IV N_2 - H_2 PRESSURE-CONCENTRATION DATA Reference: Gonikberg et al. (91)

Temperature	Pressure	Liq	uid	Vapo	r	K		
°K	Atm	Mole % H ₂	Mole % N ₂	iole % N ₂ Mole % H ₂		H ₂	N ₂	
79. 0	18.3	4. 2	95.8	91.0	9. 0	21.7	0. 0939	
	51.3	10.7	89. 3	93.6	6.4	8. 75	0.0717	
er e	66. 8	15.8	84. 2	92. 2	7. 8	5. 84	0. 0926	
	78.4	17.3	82.7	91.3	8. 7	5. 28	0.105	
11	94.9	19. 9	80. 1	91.5	8. 5	4.60	0.106	
11	99. 7	21, 3	78.7	90. 2	9. 8	4, 23	0.125	
11	107.4	22. 4	77.6	88.9	11.1	3. 97	0.143	
	143. 2	33. 7	66. 3	82.0	18.0	2. 43	0. 271	
n .	152.9	36. 4	63.6	80. 5	19. 5	2, 21	0.307	
11	175. 2	45. 7	54. 3	69. 7	30.3	1. 53	0. 558	
86.1	23. 3	5. 2	94.8	83.0	17.0	16.0	0, 179	
п	43.6	9.8	90. 2	86.5	13.5	8. 83	0.150	
11	102.6	25. 5	74. 5	84. 1	15.9	3, 30	0. 213	
n .	121.9	33.7	66.3	80.1	19.9	2.38	0.300	
n .	129.7	37. 5	62. 5	77.0	23. 0	2, 05	0.368	
u .	136.5	43.0	57. 0	56. 6	43.4	1.32	0. 761	
95. 4	13, 1	2. 7	97. 3	51.6	48.4	19.1	0.497	
**	24. 9	4. 2	95.8	69. 2	30.8	16. 5	0. 322	
***	42.4	10.2	89.8	73. 0	27. 0	7. 16	0.301	
11	61.0	16. 2	83.8	73. 3	26. 7	4. 52	0.319	
H.	76. 5	22. 1	77. 9	72. 7	27.3	3, 29	0.350	
11	91.0	27.7	72.3	72. 2	27.8	2, 61	0.384	
11	109.4	39. 4	60.6	69.1	30.9	1.75	0.510	
11	115.2	41.7	58. 3	63. 5	36.5	1.52	0.626	
"	116.1	43. 2	56.8	47.3	52. 7	1.09	0.928	
109	19.0	1.8	98. 2	20.7	79.3	11.5	0.808	
11	44.9	10, 3	89.7	48. 9	51.1	4.75	0.570	
lt.	57. 1	15.6	84.4	50. 0	50.0	3, 21	0. 592	
u .	77.4	28.4	71.6	45.7	54. 3	1.61	0. 758	

N₂-H₂ PRESSURE-CONCENTRATION DATA

Table V

Reference: Ruhemann and Zinn (212)

Temperature	Pressure	Liquid	nid	Vapor		K	
°K	Atm	Mole % H ₂	Mole % N ₂	Mole % H ₂	Mole % N ₂	H ₂	N 2
78	11.9	3.1	6.96	84.0	16.0	27.1	0.165
=	20	6.8	93. 2	88. 1	11.9	13.0	0.128
=	, 25.2	7.9	92.1	88.6	11.4	11.2	0.124
=	34.8	8.6	91.4	90.3	9.7	10, 5	0.106
Ξ	50	11.4	88.6	91.7	8.3	8.04	0.0937
83	11.9	3.8	96.2	79.5	20.5	20.9	0.213
Ξ	20	5, 2	94.8	85.5	14.5	16.4	0.153
=	25.8	7.1	92.9	87.2	12.8	12, 3	0.138
=	34.8	9.7	90.3	89.0	11.0	9.18	0.122
Ξ	50	12, 4	87.6	89. 6	10.4	7.23	0.119
90	11.8	4.6	95.4	61.9	38. 1	13.5	0.399
Ξ	20	5.7	94.3	72.5	27.5	12.7	0.292
=	25.8	7.2	92.8	76.7	23.3	10.7	0. 251
=	34.8	9.6	90.1	80.0	20.0	8.08	0.222
=	50	13.6	86.4	82.2	17.8	6.04	0. 206

Table VI

N2-H2 PRESSURE-CONCENTRATION DATA

Reference: Steckel and Zinn (225)

	Pressure	Liq	uid	Vapo	r	к	
°K	Atm	Mole % H ₂	Mole % N ₂	Mole % H ₂	Mole % N ₂	H ₂	N ₂
90. 0	15.9	67. 9	32.1	3. 7	96. 3	18.4	0. 333
11	20	74. 0	26. 0	5. 2	94.8	14. 2	0.274
"	30	78. 3	21.7	7. 2	92.8	10.9	0.234
11	38. 9	81.0	19.0	10.0	90. 0	8.10	0. 211
11	48.7	81.5	18.5	12.6	87.4	6.47	0.212
11	58. 7	82. 5	17.5	15.6	84. 4	5, 29	0.207
11	68.7	82.4	17.6	17.7	82. 3	4.66	0.214
п	78.8	80.1	19.9	21.7	78. 3	3.69	0. 254
11	88.8	80. 0	20. 0	25, 3	74.7	3.16	0. 268
11	94.3	79.0	21.0	27. 3	72.7	2. 89	0. 289
107.7	29.9	41.9	58. 1	7. 3	92, 7	5.74	0.627
11	34.6	45. 3	54.7	8. 3	91.7	5.46	0. 597
11	41.6	49. 2	50.8	11.6	88.4	4. 24	0. 575
"1	49.4	51.5	48. 5	12.7	87.3	4.06	0. 556
Ir	59.1	54. 8	45. 2	17. 3	82. 7	3. 17	0. 547
11	69. 2	52. 8	47. 2	22. 1	77. 9	2. 39	0.606
н	79.1	51.8	48. 2	27. 7	72.3	1.87	0.667
п	84.0	49. 9	50. 1	30. 1	69. 9	1.66	0. 717
	(90. 9)	(38. 9)	(61.1)	(38. 9)	(61.1)	(1.00)	(1.00)
113	24.7	18.8	81.2	3. 6	96.4	5. 22	0.842
n	39. 9	33. 4	66.6	8.3	91.7	4.02	0.726
11	69.8	39. 8	60.2	23.0	77.0	1.73	0. 782
H	74.4	35.7	64.3	32, 3	67. 7	1.11	0. 950

Table VII ${\rm N_2\text{-}H_2} \ {\rm PRESSURE\text{-}EQUILIBRIUM\ CONSTANT\ DATA }$ Reference: Akers and Eubanks (4)

ſ	Tempe	erature	Pressure		K
	°F	°K	Atm	H ₂	N ₂
	-310	83. 3	1.77		(1.0)
	11	11	2.04		(0.9)
	11	11	2.72		(0.73)
١	11	11	3.40		(0.62)
ļ	11	11	4. 08	89	(0.51)
	11	Ħ	4. 76	80	(0.45)
	11	tt	5. 44	70	(0.40)
	11	11	6.12	65	(0.36)
	11	ff	6.80	57	(0.35)
	11	11	13.6	20	(0.19)
	11	tt	20. 4	19	(0.14)
	11	11	27. 2	15	0.12
	11	Ħ	34. 0	11.5	0.11
	11	Ħ	40.8	9. 7	0.11
	n .	11	47. 6	8.2	0.105
	11	TT.	54. 4	7. 4	0.11
	11	11	61.2	6.0	0.12
	11	11	68. 0	5. 7	0.13
	tt	11	136. 1	2. 1	0.37
	11	11	(170.1)	(1.0)	(1.0)
	-240	122.2	27. 2	4.9	(1.0)
	11	11	34. 0	3. 1	0.94
	11	**	40.8	(1.7)	0.97
	11	11	(42.5)	(1.0)	(1.0)
L					

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Table VIII

SOLUBILITY OF N₂ IN H₂

Reference: Petit (196)

Temperature		I	Liquid Ph	ase Conce	entration	
°K	35 Atm.	30 Atm	25 Atm	20 Atm	15 Atm.	12. 5 Atm
	ppm N ₂					
20. 2	2	2	2	2	2	2
24.8	5. 2	5. 2	5. 2			
27.3	17	17	17	13	9	4
29.3	43	43	40. 2	30	10.5	4
30.7	75. 5		65	36.3	10.5	4
32	101	95	85	39.6	10.5	4
L	l	L				Ĺ

GAS-SOLID EQUILIBRIA

Table IX

Reference: Dokoupil, Van Soest, and Swenker (57)

Hydroge	n-Nitrogen Isobar at 50	Atm .
Temperature °K	Partial Pressure of N ₂	Vapor Phase Composition Mole % N
70.4 69.6 68.6 64.9 60.2 55.2 55.1 47.2 35.1 25.1	1210 1140 1080 695 425 250 236 82.9 16.7 6.8 6.1	3.18 3.01 2.86 1.83 1.12 0.658 0.620 0.218 0.044 0.018 0.016
	l -Nitrogen Isobar at 25 A	
69. 4 65. 5 65. 2 60. 3 59. 9 59. 9 56. 4 56. 2 53. 4 53. 4 44. 3 42. 1 38. 9 33. 2 31. 7	628 330 326 143 137 137 65.6 67.5 38.7 35.3 4.15 3.16 2.50 2.11 1.70	3.30 1.73 1.72 0.753 0.722 0.723 0.346 0.356 0.204 0.186 0.0219 0.0167 0.0131 0.0111 0.00899

Continued

Hydrog	en-Nitrogen Isobar at 15	Atm.
Temperature	Partial Pressure of N	
°K	mm Hg	tion Mole % N ₂
62.3	133	1.17
60.0	88.6	0.778
59.0	64.6	0.567
57.4	50.4	0.441
55.0	34.0	0.298
50.1	7.40	0.065
43.9	1.26	0.0111
38.0	0.211	0.00185
36.1	0.150	0.00132
34.6	0.125	0.00110
32.1	0. 137	0.00120
Hydroge	en-Nitrogen Isobar at 10	Atm.
61.8	102	1.34
60.4	74.3	0.977
58.2	47.3	0.630
56.6	33.6	0.443
54.8	24.0	0.316
50.2	6. 15	0.0809
42.2	0.455	0.00558
38.2	0.0848	0.00112
34.7	0.0316	0.000416
31.9	0.0139	0.000183
29.8	0.00900	0.000118
29.6	0.00885	0.000117

Continued

Hydr	ogen-Nitrogen Isobar at	5 Atm.
Temperature	Partial Pressure of N	Vapor Phase Composi-
°K	mm Hg	tion Mole % N ₂
60.9	71.5	1.88
60.8	63.2	1.67
57.8	34.2	0 . 902
56.7	26.0	0.685
54.8	18.3	0 . 482
50.2	5.40	0.142
42.4	0.300	0.00790
38.1	0.0316	0.000832
34:9	0.00625	0.000164
31.6	0.00322	0.0000846
30.2	0.00288	0.0000758
28.0	0.00219	0.0000577
Hydro	ogen-Nitrogen Isobar at	1.3 Atm.
60.1	59.5	6.04
59.2	40.0	4.05
58.0	29.0	2.93
49.1	2.08	0.211
45.3	0.530	0.0537
39. 1	0.0334	0.00339
35.9	0.00707	0.000717
34. 1	0.00198	0.000201

Table X

GAS-SOLID EQUILIBRIA

References: Dokoupil, Van Soest and Swenker (57)

Table IX, this report

Pressure				100 y, 1	100 y, Mole Percent N ₂ in Gas	t N ₂ in Gas				
Atm	25°K	30°K	35°K	40°K	45°K	50°K	55°K	M.09	65°K	70°K
1.3	i	;	0,00040	0.0051	0.0470	0.285	1,36	5.10	:	1 1
ហ	-	0.000069	0,000172	0. 00225	0.0227	0. 132	0.490	1.45	:	;
10	1	0.000123	0.000405	0.00220	0.0150	0,0760	0.304	0.930	1 1	!
15	!!!	!	0.00122	0.00295	0.0160	0.0720	0.279	0.790	1 1	1
25	1 1	0.0000	0.0108	0.0140	0.0248	0.0920	0.272	0.700	1.68	3.54
50	0.0169	0.0255	0.0435	0.0840	0.167	0.329	0.620	1.13	1.93	3, 12





1.5. DEPARTMENT OF COMMERCE Luther H. Hodges, Secretary

NATIONAL BUREAU OF STANDARDS A. V. Astin, Director



THE NATIONAL BUREAU OF STANDARDS

The scope of activities of the National Bureau of Standards at its major laboratories in Washington, D.C., and Boulder, Colorado, is suggested in the following listing of the divisions and sections engaged in acchnical work. In general, each section carries out specialized research, development, and engineering in the field indicated by its title. A brief description of the activities, and of the resultant publications, appears on the inside of the front cover.

WASHINGTON, D.C.

Flectricity. Resistance and Reactance. Electroehemistry. Electrical Instruments. Magnetic Measurements. Dielectrics.

Metrology. Photometry and Colorimetry. Refractometry. Photographic Research. Length. Engineering Metrology. Mass and Scale. Volumetry and Densimetry.

Heat. Temperature Physics. Heat Measurements. Cryogenie Physics. Equation of State. Statistical Physics. Radiation Physics. X-ray. Radioactivity. Radiation Theory. High Energy Radiation. Radiological Equipment. Nucleonic Instrumentation. Neutron Physics.

Analytical and Inorganic Chemistry. Pure Substances. Spectrochemistry. Solution Chemistry. Analytical Chemistry. Inorganic Chemistry.

Mechanics, Sound. Pressure and Vacuum. Fluid Mechanics. Engineering Mechanics. Rheology. Combustion

Organic and Fibrous Materiuls. Rubber. Textiles. Paper. Leather. Testing and Specifications. Polymer Structure. Plastics. Dental Research.

Metallurgy. Thermal Metallurgy. Chemical Metallurgy. Mechanical Metallurgy. Corrosion. Metal Physics'
Mineral Products. Engineering Ceramics. Glass. Refractories. Enameled Metals. Crystal Growth.
Physical Properties. Constitution and Microstructure.

Building Research. Structural Engineering. Fire Research. Mechanical Systems. Organic Building Materials, Codes and Safety Standards. Heat Transfer. Inorganie Building Materials.

Applied Mathematics. Numerical Analysis. Computation. Statistical Engineering. Mathematical Physics.

Data Processing Systems. Components and Techniques. Digital Circuitry. Digital Systems. Analog Systems. Applications Engineering.

Atomic Physics. Spectroscopy. Radiometry. Solid State Physics. Electron Physics. Atomic Physics.

Instrumentation. Engineering Electronics. Electron Devices. Electronic Instrumentation. Mechanical Instruments. Basic Instrumentation.

Physical Chemistry, Thermochemistry, Surface Chemistry, Organic Chemistry, Molecular Spectroscopy, Molecular Kinetics, Mass Spectrometry, Molecular Structure and Radiation Chemistry.

· Office of Weights and Measures.

BOULDER, COLO.

Cryogenic Engineering. Cryogenic Equipment. Cryogenic Processes. Properties of Materials. Gas Liquefaction. Ionosphere Research and Propagation. Low Frequency and Very Low Frequency Research. Ionosphere Research. Prediction Services. Sun-Earth Relationships. Field Engineering. Radio Warning Services.

Radio Propagation Engineering. Data Reduction Instrumentation. Radio Noise. Tropospheric Measurements. Tropospheric Analysis. Propagation-Terrain Effects. Radio-Meteorology. Lower Atmosphere Physics.

Radio Standards. High Frequency Electrical Standards. Radio Broadcast Service. Radio and Microwave Materials. Atomic Frequency and Time Interval Standards. Electronic Calibration Center. Millimeter-Wave Research. Microwave Circuit Standards.

Radio Systems. High Frequency and Very High Frequency Research. Modulation Research. Antenna Research. Navigation Systems. Space Telecommunications.

Upper Atmosphere and Space Physics. Upper Atmosphere and Plasma Physics. Ionosphere and Exosphere Scatter. Airglow and Aurora. Ionospheric Radio Astronomy.

